

# SOIL MECHANICS SOLUTIONS MANUAL



**R.F. CRAIG**

[Download full file from buklibry.com](https://buklibry.com)

SPRINGER-SCIENCE+  
BUSINESS MEDIA, B.V.



# **Soil Mechanics Fifth Edition Solutions Manual**

**R.F. Craig**

**Department of Civil Engineering  
University of Dundee, UK**



**SPRINGER-SCIENCE+BUSINESS MEDIA, B.V.**

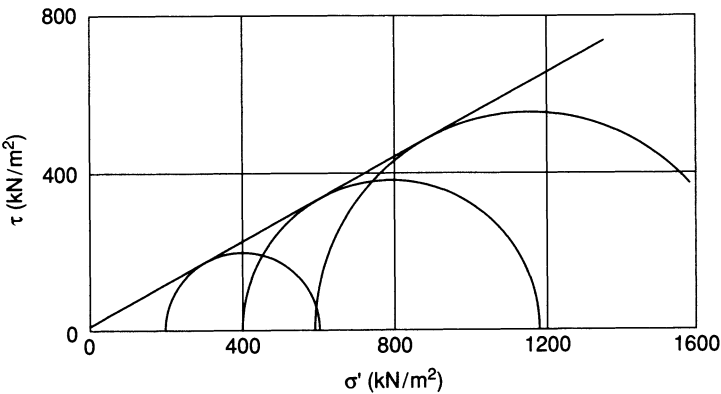


Fig. Q4.6

4.6

$\sigma'_3$ (kN/m <sup>2</sup> )	$\Delta V/V_0$	$\Delta l/l_0$	Area (mm <sup>2</sup> )	Load (N)	$\sigma_1 - \sigma_3$ (kN/m <sup>2</sup> )	$\sigma'_1$ (kN/m <sup>2</sup> )
200	0.061	0.095	1177	480	408	608
400	0.086	0.110	1165	895	768	1168
600	0.108	0.124	1155	1300	1126	1726

The average cross-sectional area of each specimen is obtained from equation 4.12; the original values of  $A$ ,  $l$  and  $V$  are:  $A_0 = 1134 \text{ mm}^2$ ,  $l_0 = 76 \text{ mm}$ ,  $V_0 = 86\,200 \text{ mm}^3$ . The Mohr circles and failure envelope are drawn in Fig. Q4.6, from which  $c' = 15 \text{ kN/m}^2$  and  $\phi' = 28^\circ$ .

4.7

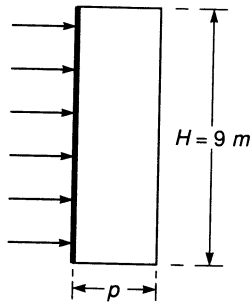
The torque required to produce shear failure is given by:

$$\begin{aligned}
 T &= \pi d h c_u \frac{d}{2} + 2 \int_0^{d/2} 2\pi r dr c_u r \\
 &= \pi c_u \frac{d^2 h}{2} + 4\pi c_u \int_0^{d/2} r^2 dr \\
 &= \pi c_u \left( \frac{d^2 h}{2} + \frac{d^3}{6} \right)
 \end{aligned}$$

Then:

$$35 = \pi c_u \left( \frac{5^2 \times 10}{2} + \frac{5^3}{6} \right) \times 10^{-3}$$

$$\therefore c_u = 76 \text{ kN/m}^2$$



**Fig. Q6.10**

**6.10**

For  $\phi' = 40^\circ$ ,  $K_a = 0.22$

The pressure distribution is shown in Fig. Q6.10.

$$p = 0.65K_a\gamma H = 0.65 \times 0.22 \times 19 \times 9 = 24.5 \text{ kN/m}^2$$

$$\text{Strut load} = 24.5 \times 1.5 \times 3 = 110 \text{ kN}$$

**6.11**

$$\gamma = 18 \text{ kN/m}^3; \quad \phi' = 34^\circ$$

$$H = 3.50 \text{ m}; \quad nH = 3.35 \text{ m}; \quad mH = 1.85 \text{ m}$$

Consider a trial value of  $F = 2.0$ . Refer to Fig. 6.33.

$$\phi'_m = \tan^{-1} \left( \frac{\tan 34^\circ}{2.0} \right) = 18.6^\circ$$

Then:

$$\alpha = 45^\circ + \frac{\phi'_m}{2} = 54.3^\circ$$

$$W = \frac{1}{2} \times 18 \times 3.50^2 \times \cot 54.3^\circ = 79.2 \text{ kN/m}$$

$$P = \frac{1}{2} \times \gamma_s \times 3.35^2 = 5.61 \gamma_s \text{ kN/m}$$

$$U = \frac{1}{2} \times 9.8 \times 1.85^2 \times \operatorname{cosec} 54.3^\circ = 20.6 \text{ kN/m}$$

Equations 6.28 and 6.29 then become:

$$5.61\gamma_s + (N - 20.6) \tan 18.6^\circ \cos 54.3^\circ - N \sin 54.3^\circ = 0$$

$$79.2 - (N - 20.6) \tan 18.6^\circ \sin 54.3^\circ - N \cos 54.3^\circ = 0$$

$$\therefore \tan \beta = 0.234$$

$$\beta = 13^\circ$$

Water table well below surface; the factor of safety is given by equation 9.11:

$$F = \frac{\tan \phi'}{\tan \beta}$$

$$= \frac{\tan 36^\circ}{\tan 13^\circ}$$

$$= 3.1$$